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## Structure Reports

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# Bis(acrylonitrile- $\kappa$ N)dichlorido( $\eta^4$ -cycloocta-1,5-diene)ruthenium(II)

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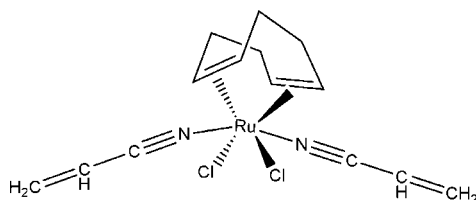
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 Key indicators: single-crystal X-ray study;  $T = 100$  K; mean  $\sigma(\text{C}-\text{C}) = 0.005$  Å; disorder in main residue;  $R$  factor = 0.033;  $wR$  factor = 0.075; data-to-parameter ratio = 18.9.

In the title complex,  $[\text{RuCl}_2(\text{C}_8\text{H}_{12})(\text{C}_3\text{H}_3\text{N})_2]$ , the metal ion is coordinated to centers of each of the double bonds of the cycloocta-1,5-diene ligand, to two chloride ions (in *cis* positions) and to two N-atom donors from two acrylonitrile molecules that complete the coordination sphere for the neutral complex. The coordination about the  $\text{Ru}^{\text{II}}$  atom can thus be considered octahedral with slight trigonal distortion. The three C atoms of one of the acrylonitrile ligands are disordered over two sets of sites in a 0.581 (13):0.419 (13) ratio.

## Related literature

For a review of related compounds, see: Chiririwa *et al.* (2011). For the synthesis of starting materials, see: Ashworth *et al.* (1987)



## Experimental

## Crystal data

 $[\text{RuCl}_2(\text{C}_8\text{H}_{12})(\text{C}_3\text{H}_3\text{N})_2]$   
 $M_r = 386.27$   
 Monoclinic,  $P2_1/c$   
 $a = 7.1079$  (8) Å  
 $b = 26.818$  (3) Å  
 $c = 8.1555$  (10) Å  
 $\beta = 101.408$  (2)°

 $V = 1523.9$  (3) Å<sup>3</sup>  
 $Z = 4$   
 Mo  $K\alpha$  radiation  
 $\mu = 1.37$  mm<sup>-1</sup>  
 $T = 100$  K  
 $0.22 \times 0.09 \times 0.04$  mm

## Data collection

 Bruker APEX2 CCD  
 diffractometer  
 12653 measured reflections

 3776 independent reflections  
 3093 reflections with  $I > 2\sigma(I)$   
 $R_{\text{int}} = 0.040$ 

## Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.033$   
 $wR(F^2) = 0.075$   
 $S = 1.03$   
 3776 reflections

 200 parameters  
 H-atom parameters constrained  
 $\Delta\rho_{\text{max}} = 1.14$  e Å<sup>-3</sup>  
 $\Delta\rho_{\text{min}} = -1.11$  e Å<sup>-3</sup>

Data collection: APEX2 (Bruker, 2007); cell refinement: SAINT-Plus (Bruker, 2007); data reduction: SAINT-Plus and XPREP (Bruker, 2007); program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: DIAMOND (Brandenburg & Putz, 2005) and ORTEP-3 (Farrugia, 1997); software used to prepare material for publication: WinGX (Farrugia, 1999).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: JH2321).

## References

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**supplementary materials**

*Acta Cryst.* (2011). E67, m1335 [ doi:10.1107/S1600536811035380 ]

## Bis(acrylonitrile- $\kappa$ N)dichlorido( $\eta^4$ -cycloocta-1,5-diene)ruthenium(II)

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### Comment

The present ruthenium complex, Fig.1, has been synthesized in a similar way as done earlier for the acetonitrile derivative (Chiririwa *et al.* 2011). Organonitrile solvate complexes are widely useful for synthesis of organometallic compounds because of facile substitution at the solvate coordination sites. Similarly, 1,5-cyclooctadiene complexes have found considerable use in organometallic chemistry as well.

The two acrylonitrile ligands are not *trans* to each other, as the N(2)—Ru—N(1) angle is 164.62 (11) $^\circ$  whereas the same angle is 163.15 (6) $^\circ$  in the acetonitrile derivative. This is attributed to repulsion by the alkene bonds of the COD ligand. One of the acrylonitrile ligands is slightly bent as we observed earlier in the acetonitrile derivative. The N(2)—C(21)—C(22) bond angle is 179.2 (3) $^\circ$ . This is probably due to packing forces.

It turned out that in the crystal structure the disorder involves three carbon atoms between the 3 positions with site occupation factors of 84:16. A 11 alternative positions refined quite well without any kind of restraints and the C atoms assume positions that make an almost symmetrical system.

### Experimental

A suspension of [ $\{\text{RuCl}_2(\text{COD})\}_x$ ] (0.5 g) in acrylonitrile (25 ml) was refluxed for 12 h. The orange solution was filtered hot and concentrated on a steam bath to half volume and cooled to 0  $^\circ\text{C}$  overnight affording orange crystals in 50% yield suitable for X-ray diffraction studies.

### Refinement

The methylene, and methyl H atoms were placed in geometrically idealized positions (C—H = 0.95–0.98) and constrained to ride on their parent atoms with  $U_{\text{iso}}(\text{H}) = 1.2U_{\text{eq}}(\text{C})$  for methylene H atoms, and  $U_{\text{iso}}(\text{H}) = 1.5U_{\text{eq}}(\text{C})$  for methyl H atoms respectively. The acrylonitrile ligand is disordered over 3 well resolved positions. The disorder involves three C atoms which assume positions that make an almost symmetrical system. Unfortunately this disorder could not be resolved.

### Figures

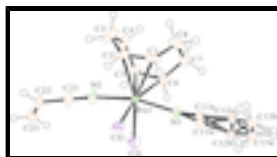


Fig. 1. The structure of the title compound, showing 50% probability displacement ellipsoids. For the C atoms, the first digit indicates ring number and the second digit indicates the position of the atom in the ring. Some labels have been omitted for clarity.

## Bis(acrylonitrile- $\kappa$ N)dichlorido( $\eta^4$ -cycloocta-1,5-diene)ruthenium(II)

### Crystal data

|  |   |
|--|---|
| [RuCl <sub>2</sub> (C <sub>8</sub> H <sub>12</sub> )(C <sub>3</sub> H <sub>3</sub> N) <sub>2</sub> ] | $F(000) = 776$  |
| $M_r = 386.27$   | $D_x = 1.684 \text{ Mg m}^{-3}$                         |
| Monoclinic, $P2_1/c$   | Mo $K\alpha$ radiation, $\lambda = 0.71073 \text{ \AA}$ |
| Hall symbol: -P 2ybc   | Cell parameters from 3596 reflections                   |
| $a = 7.1079 (8) \text{ \AA}$   | $\theta = 2.7\text{--}28.2^\circ$                       |
| $b = 26.818 (3) \text{ \AA}$   | $\mu = 1.37 \text{ mm}^{-1}$                            |
| $c = 8.1555 (10) \text{ \AA}$  | $T = 100 \text{ K}$                                     |
| $\beta = 101.408 (2)^\circ$  | Rectangular, orange                                     |
| $V = 1523.9 (3) \text{ \AA}^3$   | $0.22 \times 0.09 \times 0.04 \text{ mm}$               |
| $Z = 4$  |   |

### Data collection

|   |  |
|---|--|
| Bruker APEXII CCD diffractometer                  | 3093 reflections with $I > 2\sigma(I)$                                 |
| Radiation source: fine-focus sealed tube graphite | $R_{\text{int}} = 0.040$   |
| $\varphi$ and $\omega$ scans                      | $\theta_{\text{max}} = 28.3^\circ$ , $\theta_{\text{min}} = 1.5^\circ$ |
| 12653 measured reflections                        | $h = -9 \rightarrow 8$   |
| 3776 independent reflections                      | $k = -35 \rightarrow 35$   |
|   | $l = -10 \rightarrow 10$   |

### Refinement

|                                 |  |
|---------------------------------|--|
| Refinement on $F^2$             | Primary atom site location: structure-invariant direct methods |
| Least-squares matrix: full      | Secondary atom site location: difference Fourier map           |
| $R[F^2 > 2\sigma(F^2)] = 0.033$ | Hydrogen site location: inferred from neighbouring sites       |
| $wR(F^2) = 0.075$               | H-atom parameters constrained                                  |
| $S = 1.03$                      | $w = 1/[\sigma^2(F_o^2) + (0.0254P)^2 + 2.2348P]$              |
| 3776 reflections                | where $P = (F_o^2 + 2F_c^2)/3$                                 |
| 200 parameters                  | $(\Delta/\sigma)_{\text{max}} = 0.001$                         |
| 0 restraints                    | $\Delta\rho_{\text{max}} = 1.14 \text{ e \AA}^{-3}$            |
|                                 | $\Delta\rho_{\text{min}} = -1.11 \text{ e \AA}^{-3}$           |

### Special details

**Geometry.** All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement.** Refinement of  $F^2$  against ALL reflections. The weighted  $R$ -factor  $wR$  and goodness of fit  $S$  are based on  $F^2$ , conventional  $R$ -factors  $R$  are based on  $F$ , with  $F$  set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating  $R$ -factors(gt) *etc.* and is not relevant to the choice of reflections for refinement.  $R$ -factors based on  $F^2$  are statistically about twice as large as those based on  $F$ , and  $R$ -factors based on ALL data will be even larger. The Following Model and Quality ALERTS were generated -(Acta-Mode) <<< Format: alert-number\_ALERT\_alert-type\_alert-level text 912\_ALERT\_4\_C Missing # of FCF Reflections Above STh/L= 0.600 7 Noted.

*Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters ( $\text{\AA}^2$ )*

|      | <i>x</i>     | <i>y</i>     | <i>z</i>     | $U_{\text{iso}}^*/U_{\text{eq}}$ | Occ. (<1)  |
|------|--------------|--------------|--------------|----------------------------------|------------|
| Ru1  | 0.50503 (3)  | 0.634032 (9) | 0.06561 (3)  | 0.01778 (7)                      |            |
| C11  | 0.75368 (12) | 0.59883 (4)  | 0.27841 (13) | 0.0487 (3)                       |            |
| C12  | 0.39293 (11) | 0.68818 (3)  | 0.26070 (9)  | 0.02385 (16)                     |            |
| C1   | 0.3571 (5)   | 0.67769 (12) | -0.1549 (4)  | 0.0284 (7)                       |            |
| H1   | 0.3868       | 0.7064       | -0.0866      | 0.034*                           |            |
| C2   | 0.2289 (4)   | 0.64408 (13) | -0.1127 (4)  | 0.0286 (7)                       |            |
| H2   | 0.1739       | 0.6513       | -0.0182      | 0.034*                           |            |
| C3   | 0.1699 (5)   | 0.59630 (15) | -0.2071 (5)  | 0.0404 (9)                       |            |
| H3A  | 0.088        | 0.6047       | -0.3165      | 0.048*                           |            |
| H3B  | 0.0917       | 0.5762       | -0.1436      | 0.048*                           |            |
| C4   | 0.3393 (5)   | 0.56453 (14) | -0.2372 (5)  | 0.0403 (9)                       |            |
| H4A  | 0.3016       | 0.529        | -0.2387      | 0.048*                           |            |
| H4B  | 0.3651       | 0.5727       | -0.3491      | 0.048*                           |            |
| C5   | 0.5230 (4)   | 0.57127 (12) | -0.1091 (5)  | 0.0283 (7)                       |            |
| H5   | 0.5447       | 0.5507       | -0.0124      | 0.034*                           |            |
| C6   | 0.6595 (4)   | 0.60595 (13) | -0.1271 (4)  | 0.0273 (7)                       |            |
| H6   | 0.7733       | 0.6072       | -0.0434      | 0.033*                           |            |
| C7   | 0.6410 (5)   | 0.64203 (13) | -0.2703 (4)  | 0.0333 (8)                       |            |
| H7A  | 0.6502       | 0.6233       | -0.373       | 0.04*                            |            |
| H7B  | 0.7503       | 0.6656       | -0.2476      | 0.04*                            |            |
| C8   | 0.4539 (6)   | 0.67198 (14) | -0.3029 (4)  | 0.0369 (9)                       |            |
| H8A  | 0.4812       | 0.7057       | -0.3421      | 0.044*                           |            |
| H8B  | 0.3627       | 0.6557       | -0.3947      | 0.044*                           |            |
| C23  | 0.2232 (5)   | 0.48525 (13) | 0.3860 (4)   | 0.0343 (8)                       |            |
| H23A | 0.3572       | 0.4795       | 0.3995       | 0.041*                           |            |
| H23B | 0.1468       | 0.4638       | 0.4388       | 0.041*                           |            |
| N1   | 0.6921 (4)   | 0.68978 (11) | 0.0491 (3)   | 0.0305 (7)                       |            |
| C11A | 0.7543 (16)  | 0.7291 (4)   | 0.0267 (11)  | 0.0137 (18)                      | 0.419 (13) |
| C12A | 0.8507 (12)  | 0.7726 (3)   | -0.0172 (8)  | 0.015 (2)                        | 0.419 (13) |
| H12A | 0.7749       | 0.8          | -0.0659      | 0.018*                           | 0.419 (13) |
| C13A | 1.0368 (13)  | 0.7766 (3)   | 0.0062 (10)  | 0.022 (2)                        | 0.419 (13) |
| H13A | 1.116        | 0.7498       | 0.0546       | 0.027*                           | 0.419 (13) |
| H13B | 1.0932       | 0.8063       | -0.0253      | 0.027*                           | 0.419 (13) |
| C11B | 0.8206 (11)  | 0.7163 (3)   | 0.0505 (9)   | 0.0170 (14)                      | 0.581 (13) |
| C12B | 0.9662 (8)   | 0.7536 (2)   | 0.0446 (6)   | 0.0183 (17)                      | 0.581 (13) |
| H12B | 1.0946       | 0.7477       | 0.1006       | 0.022*                           | 0.581 (13) |
| C13B | 0.9232 (10)  | 0.7954 (3)   | -0.0371 (7)  | 0.0249 (18)                      | 0.581 (13) |
| H13C | 0.7951       | 0.8016       | -0.0934      | 0.03*                            | 0.581 (13) |

## supplementary materials

|      |            |              |            |            |            |
|------|------------|--------------|------------|------------|------------|
| H13D | 1.0202     | 0.8196       | -0.04      | 0.03*      | 0.581 (13) |
| N2   | 0.3376 (4) | 0.58267 (10) | 0.1480 (4) | 0.0267 (6) |            |
| C21  | 0.2527 (5) | 0.55592 (12) | 0.2127 (4) | 0.0277 (7) |            |
| C22  | 0.1436 (5) | 0.52268 (13) | 0.2946 (4) | 0.0288 (7) |            |
| H22  | 0.0094     | 0.5279       | 0.2824     | 0.035*     |            |

### Atomic displacement parameters ( $\text{\AA}^2$ )

|      | $U^{11}$     | $U^{22}$     | $U^{33}$     | $U^{12}$     | $U^{13}$     | $U^{23}$     |
|------|--------------|--------------|--------------|--------------|--------------|--------------|
| Ru1  | 0.01229 (11) | 0.01244 (12) | 0.02730 (13) | -0.00135 (9) | 0.00074 (8)  | 0.00569 (10) |
| C11  | 0.0245 (4)   | 0.0659 (7)   | 0.0537 (6)   | 0.0169 (4)   | 0.0029 (4)   | 0.0357 (5)   |
| C12  | 0.0281 (4)   | 0.0196 (4)   | 0.0208 (3)   | -0.0016 (3)  | -0.0026 (3)  | 0.0012 (3)   |
| C1   | 0.0391 (18)  | 0.0215 (16)  | 0.0185 (14)  | 0.0115 (14)  | -0.0093 (13) | -0.0031 (12) |
| C2   | 0.0191 (14)  | 0.0326 (19)  | 0.0292 (16)  | 0.0094 (13)  | -0.0074 (12) | -0.0133 (14) |
| C3   | 0.0209 (16)  | 0.048 (2)    | 0.051 (2)    | -0.0056 (16) | 0.0036 (15)  | -0.0299 (19) |
| C4   | 0.0284 (17)  | 0.032 (2)    | 0.066 (2)    | -0.0121 (16) | 0.0226 (17)  | -0.0284 (19) |
| C5   | 0.0253 (16)  | 0.0136 (15)  | 0.052 (2)    | 0.0035 (13)  | 0.0211 (14)  | -0.0012 (14) |
| C6   | 0.0191 (14)  | 0.0271 (18)  | 0.0379 (17)  | -0.0002 (13) | 0.0110 (13)  | 0.0002 (14)  |
| C7   | 0.042 (2)    | 0.0281 (19)  | 0.0309 (17)  | -0.0093 (16) | 0.0109 (15)  | -0.0038 (14) |
| C8   | 0.058 (2)    | 0.030 (2)    | 0.0201 (15)  | 0.0067 (18)  | 0.0004 (15)  | -0.0025 (14) |
| C23  | 0.039 (2)    | 0.0249 (18)  | 0.045 (2)    | -0.0067 (16) | 0.0227 (16)  | -0.0051 (16) |
| N1   | 0.0380 (16)  | 0.0328 (17)  | 0.0196 (12)  | -0.0209 (14) | 0.0030 (11)  | 0.0011 (12)  |
| C11A | 0.016 (5)    | 0.009 (4)    | 0.015 (4)    | 0.004 (3)    | -0.001 (3)   | 0.004 (3)    |
| C12A | 0.019 (4)    | 0.011 (4)    | 0.014 (3)    | 0.000 (3)    | 0.004 (3)    | 0.000 (3)    |
| C13A | 0.020 (5)    | 0.019 (4)    | 0.026 (4)    | -0.005 (4)   | -0.001 (3)   | 0.003 (3)    |
| C11B | 0.017 (3)    | 0.016 (4)    | 0.017 (3)    | 0.007 (3)    | -0.001 (2)   | 0.000 (2)    |
| C12B | 0.014 (3)    | 0.018 (3)    | 0.021 (3)    | -0.002 (2)   | -0.001 (2)   | -0.002 (2)   |
| C13B | 0.023 (3)    | 0.029 (4)    | 0.021 (3)    | -0.005 (3)   | 0.001 (2)    | 0.001 (3)    |
| N2   | 0.0216 (13)  | 0.0173 (14)  | 0.0450 (16)  | -0.0011 (11) | 0.0155 (12)  | -0.0004 (12) |
| C21  | 0.0246 (16)  | 0.0177 (16)  | 0.0448 (19)  | -0.0023 (13) | 0.0163 (14)  | -0.0074 (14) |
| C22  | 0.0235 (16)  | 0.0261 (18)  | 0.0420 (18)  | -0.0075 (14) | 0.0191 (14)  | -0.0071 (15) |

### Geometric parameters ( $\text{\AA}$ , $^\circ$ )

|         |            |           |            |
|---------|------------|-----------|------------|
| Ru1—N2  | 2.021 (3)  | C7—C8     | 1.532 (5)  |
| Ru1—N1  | 2.023 (3)  | C7—H7A    | 0.99       |
| Ru1—C2  | 2.216 (3)  | C7—H7B    | 0.99       |
| Ru1—C6  | 2.219 (3)  | C8—H8A    | 0.99       |
| Ru1—C5  | 2.225 (3)  | C8—H8B    | 0.99       |
| Ru1—C1  | 2.228 (3)  | C23—C22   | 1.310 (5)  |
| Ru1—C12 | 2.4035 (8) | C23—H23A  | 0.95       |
| Ru1—C11 | 2.4111 (9) | C23—H23B  | 0.95       |
| C1—C2   | 1.373 (5)  | N1—C11B   | 1.156 (7)  |
| C1—C8   | 1.511 (5)  | N1—C11A   | 1.171 (9)  |
| C1—H1   | 0.95       | C11A—C12A | 1.434 (13) |
| C2—C3   | 1.511 (5)  | C12A—C13A | 1.303 (14) |
| C2—H2   | 0.95       | C12A—H12A | 0.95       |
| C3—C4   | 1.534 (5)  | C13A—H13A | 0.95       |
| C3—H3A  | 0.99       | C13A—H13B | 0.95       |

|             |             |                |            |
|-------------|-------------|----------------|------------|
| C3—H3B      | 0.99        | C11B—C12B      | 1.447 (10) |
| C4—C5       | 1.513 (5)   | C12B—C13B      | 1.309 (11) |
| C4—H4A      | 0.99        | C12B—H12B      | 0.95       |
| C4—H4B      | 0.99        | C13B—H13C      | 0.95       |
| C5—C6       | 1.373 (4)   | C13B—H13D      | 0.95       |
| C5—H5       | 0.95        | N2—C21         | 1.132 (4)  |
| C6—C7       | 1.503 (5)   | C21—C22        | 1.431 (4)  |
| C6—H6       | 0.95        | C22—H22        | 0.95       |
| N2—Ru1—N1   | 164.62 (11) | C3—C4—H4B      | 108.6      |
| N2—Ru1—C2   | 78.32 (13)  | H4A—C4—H4B     | 107.5      |
| N1—Ru1—C2   | 112.03 (13) | C6—C5—C4       | 122.6 (3)  |
| N2—Ru1—C6   | 114.26 (11) | C6—C5—Ru1      | 71.78 (19) |
| N1—Ru1—C6   | 77.28 (12)  | C4—C5—Ru1      | 112.4 (2)  |
| C2—Ru1—C6   | 94.29 (12)  | C6—C5—H5       | 118.7      |
| N2—Ru1—C5   | 79.02 (11)  | C4—C5—H5       | 118.7      |
| N1—Ru1—C5   | 113.25 (12) | Ru1—C5—H5      | 85.9       |
| C2—Ru1—C5   | 80.06 (12)  | C5—C6—C7       | 124.3 (3)  |
| C6—Ru1—C5   | 35.98 (11)  | C5—C6—Ru1      | 72.24 (19) |
| N2—Ru1—C1   | 114.32 (13) | C7—C6—Ru1      | 110.7 (2)  |
| N1—Ru1—C1   | 76.67 (12)  | C5—C6—H6       | 117.8      |
| C2—Ru1—C1   | 36.00 (13)  | C7—C6—H6       | 117.8      |
| C6—Ru1—C1   | 80.07 (12)  | Ru1—C6—H6      | 87.1       |
| C5—Ru1—C1   | 87.62 (12)  | C6—C7—C8       | 114.3 (3)  |
| N2—Ru1—C12  | 84.11 (8)   | C6—C7—H7A      | 108.7      |
| N1—Ru1—C12  | 84.59 (9)   | C8—C7—H7A      | 108.7      |
| C2—Ru1—C12  | 89.67 (9)   | C6—C7—H7B      | 108.7      |
| C6—Ru1—C12  | 161.63 (9)  | C8—C7—H7B      | 108.7      |
| C5—Ru1—C12  | 161.70 (8)  | H7A—C7—H7B     | 107.6      |
| C1—Ru1—C12  | 92.95 (9)   | C1—C8—C7       | 115.6 (3)  |
| N2—Ru1—C11  | 83.67 (8)   | C1—C8—H8A      | 108.4      |
| N1—Ru1—C11  | 86.52 (9)   | C7—C8—H8A      | 108.4      |
| C2—Ru1—C11  | 161.43 (10) | C1—C8—H8B      | 108.4      |
| C6—Ru1—C11  | 88.96 (9)   | C7—C8—H8B      | 108.4      |
| C5—Ru1—C11  | 92.18 (10)  | H8A—C8—H8B     | 107.4      |
| C1—Ru1—C11  | 161.56 (10) | C22—C23—H23A   | 120        |
| C12—Ru1—C11 | 92.97 (3)   | C22—C23—H23B   | 120        |
| C2—C1—C8    | 124.3 (3)   | H23A—C23—H23B  | 120        |
| C2—C1—Ru1   | 71.52 (18)  | C11B—N1—Ru1    | 169.3 (5)  |
| C8—C1—Ru1   | 112.0 (2)   | C11A—N1—Ru1    | 161.6 (6)  |
| C2—C1—H1    | 117.9       | N1—C11A—C12A   | 170.1 (10) |
| C8—C1—H1    | 117.9       | C13A—C12A—C11A | 123.5 (9)  |
| Ru1—C1—H1   | 86.4        | C13A—C12A—H12A | 118.3      |
| C1—C2—C3    | 124.1 (3)   | C11A—C12A—H12A | 118.3      |
| C1—C2—Ru1   | 72.48 (17)  | C12A—C13A—H13A | 120        |
| C3—C2—Ru1   | 110.6 (2)   | C12A—C13A—H13B | 120        |
| C1—C2—H2    | 118         | H13A—C13A—H13B | 120        |
| C3—C2—H2    | 118         | N1—C11B—C12B   | 173.7 (8)  |
| Ru1—C2—H2   | 86.9        | C13B—C12B—C11B | 120.9 (7)  |
| C2—C3—C4    | 113.9 (3)   | C13B—C12B—H12B | 119.6      |

## supplementary materials

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| C2—C3—H3A     | 108.8       | C11B—C12B—H12B  | 119.6       |
| C4—C3—H3A     | 108.8       | C12B—C13B—H13C  | 120         |
| C2—C3—H3B     | 108.8       | C12B—C13B—H13D  | 120         |
| C4—C3—H3B     | 108.8       | H13C—C13B—H13D  | 120         |
| H3A—C3—H3B    | 107.7       | C21—N2—Ru1      | 171.8 (3)   |
| C5—C4—C3      | 114.9 (3)   | N2—C21—C22      | 179.2 (3)   |
| C5—C4—H4A     | 108.6       | C23—C22—C21     | 122.0 (3)   |
| C3—C4—H4A     | 108.6       | C23—C22—H22     | 119         |
| C5—C4—H4B     | 108.6       | C21—C22—H22     | 119         |
| N2—Ru1—C1—C2  | -0.5 (2)    | N1—Ru1—C5—C4    | -116.6 (2)  |
| N1—Ru1—C1—C2  | -169.1 (2)  | C2—Ru1—C5—C4    | -6.8 (3)    |
| C6—Ru1—C1—C2  | 111.7 (2)   | C6—Ru1—C5—C4    | -118.5 (4)  |
| C5—Ru1—C1—C2  | 76.3 (2)    | C1—Ru1—C5—C4    | -42.2 (3)   |
| Cl2—Ru1—C1—C2 | -85.38 (18) | Cl2—Ru1—C5—C4   | 49.9 (5)    |
| Cl1—Ru1—C1—C2 | 166.0 (2)   | Cl1—Ru1—C5—C4   | 156.2 (2)   |
| N2—Ru1—C1—C8  | -120.9 (2)  | C4—C5—C6—C7     | 2.2 (5)     |
| N1—Ru1—C1—C8  | 70.5 (3)    | Ru1—C5—C6—C7    | -103.3 (3)  |
| C2—Ru1—C1—C8  | -120.4 (3)  | C4—C5—C6—Ru1    | 105.5 (3)   |
| C6—Ru1—C1—C8  | -8.7 (2)    | N2—Ru1—C6—C5    | 12.6 (2)    |
| C5—Ru1—C1—C8  | -44.1 (3)   | N1—Ru1—C6—C5    | -178.2 (2)  |
| Cl2—Ru1—C1—C8 | 154.2 (2)   | C2—Ru1—C6—C5    | -66.5 (2)   |
| Cl1—Ru1—C1—C8 | 45.7 (4)    | C1—Ru1—C6—C5    | -99.7 (2)   |
| C8—C1—C2—C3   | 1.1 (5)     | Cl2—Ru1—C6—C5   | -168.5 (2)  |
| Ru1—C1—C2—C3  | -103.4 (3)  | Cl1—Ru1—C6—C5   | 95.1 (2)    |
| C8—C1—C2—Ru1  | 104.5 (3)   | N2—Ru1—C6—C7    | 133.4 (2)   |
| N2—Ru1—C2—C1  | 179.5 (2)   | N1—Ru1—C6—C7    | -57.4 (2)   |
| N1—Ru1—C2—C1  | 11.4 (2)    | C2—Ru1—C6—C7    | 54.3 (2)    |
| C6—Ru1—C2—C1  | -66.6 (2)   | C5—Ru1—C6—C7    | 120.8 (3)   |
| C5—Ru1—C2—C1  | -99.8 (2)   | C1—Ru1—C6—C7    | 21.1 (2)    |
| Cl2—Ru1—C2—C1 | 95.47 (18)  | Cl2—Ru1—C6—C7   | -47.7 (4)   |
| Cl1—Ru1—C2—C1 | -166.1 (2)  | Cl1—Ru1—C6—C7   | -144.0 (2)  |
| N2—Ru1—C2—C3  | -59.9 (3)   | C5—C6—C7—C8     | 51.7 (5)    |
| N1—Ru1—C2—C3  | 132.0 (3)   | Ru1—C6—C7—C8    | -30.5 (3)   |
| C6—Ru1—C2—C3  | 54.0 (3)    | C2—C1—C8—C7     | -87.3 (4)   |
| C5—Ru1—C2—C3  | 20.8 (3)    | Ru1—C1—C8—C7    | -5.3 (4)    |
| C1—Ru1—C2—C3  | 120.6 (3)   | C6—C7—C8—C1     | 24.1 (4)    |
| Cl2—Ru1—C2—C3 | -144.0 (3)  | N2—Ru1—N1—C11B  | 72 (2)      |
| Cl1—Ru1—C2—C3 | -45.6 (4)   | C2—Ru1—N1—C11B  | -157 (2)    |
| C1—C2—C3—C4   | 50.4 (5)    | C6—Ru1—N1—C11B  | -68 (2)     |
| Ru1—C2—C3—C4  | -31.9 (4)   | C5—Ru1—N1—C11B  | -69 (2)     |
| C2—C3—C4—C5   | 27.1 (5)    | C1—Ru1—N1—C11B  | -150 (2)    |
| C3—C4—C5—C6   | -90.6 (4)   | Cl2—Ru1—N1—C11B | 115 (2)     |
| C3—C4—C5—Ru1  | -8.5 (4)    | Cl1—Ru1—N1—C11B | 22 (2)      |
| N2—Ru1—C5—C6  | -168.3 (2)  | N2—Ru1—N1—C11A  | -101.0 (15) |
| N1—Ru1—C5—C6  | 1.9 (2)     | C2—Ru1—N1—C11A  | 29.3 (15)   |
| C2—Ru1—C5—C6  | 111.8 (2)   | C6—Ru1—N1—C11A  | 118.8 (15)  |
| C1—Ru1—C5—C6  | 76.3 (2)    | C5—Ru1—N1—C11A  | 117.7 (15)  |
| Cl2—Ru1—C5—C6 | 168.5 (2)   | C1—Ru1—N1—C11A  | 36.2 (15)   |
| Cl1—Ru1—C5—C6 | -85.2 (2)   | Cl2—Ru1—N1—C11A | -58.1 (15)  |



N2—Ru1—C5—C4

73.1 (3)

Cl1—Ru1—N1—C11A

-151.4 (15)

Fig. 1

